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Focussing and normal mode scattering of the first mode internal tide by mesoscale eddy interaction

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Workshop on Sub-mesoscale Ocean Processes

Michael Dunphy

Focussing and normal mode scattering

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## Introduction

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Internal tides					

• There are a variety of internal wave generation mechanisms

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Internal tides					

- There are a variety of internal wave generation mechanisms
- Barotropic tide-topography interaction has received a lot of attention

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Internal tides					

- There are a variety of internal wave generation mechanisms
- Barotropic tide-topography interaction has received a lot of attention
- [Bell(1975)], [Legg and Huijts(2006)], and many others
- $M_2$  internal tide generation is among the most prominent

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 $M_2$  internal tide generation: (Simmons, 2004), two layer model



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## • The fate of the internal tide is still under investigation

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- The fate of the internal tide is still under investigation
  - Local dissipation vs. propagation

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- The fate of the internal tide is still under investigation
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  - Wave-wave-vortex resonance has been looked at by [Lelong and Riley(1991)] and [Bartello(1995)]

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  - Wave-wave-vortex resonance has been looked at by [Lelong and Riley(1991)] and [Bartello(1995)]
  - Wave capture, [Bühler and McIntyre(2005)]

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Numerical experiment setup						

• We numerically simulate the interaction of a mode-one internal tide and an isolated mesoscale eddy

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- We numerically simulate the interaction of a mode-one internal tide and an isolated mesoscale eddy
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- Two latitude regimes:
  - Low  $(f = 0.5 \times 10^{-4} \text{ s}^{-1})$ ,  $\approx 20^{\circ} \text{N}$
  - Mid  $(f = 1.0 \times 10^{-4} \text{ s}^{-1})$ ,  $\approx 43^{\circ} \text{N}$

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• Mid 
$$(f = 1.0 \times 10^{-4} \text{ s}^{-1})$$
,  $\approx 43^{\circ} \text{N}$ 

Parameter	Value
N <sub>0</sub>	$1.0  imes 10^{-3} \ { m s}^{-1}$
Т	44712 s (one tidal period)
ω	$1.4053 imes 10^{-4}~{ m s}^{-1}~(M_2)$
$U_t$	$5 \text{ cm s}^{-1}$
g	9.81 m s <sup>-2</sup>
$ ho_0$	$1028 \ { m kg} \ { m m}^{-3}$
$\Delta t$	69 s

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Numerical experiment setup						

$$\Psi=\psi(r)\Phi(z)=-rac{5^{rac{5}{2}}}{64}U_{ heta}L_{E}\mathrm{sech}^{4}\left(rac{r}{L_{E}}
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- $L_E$  eddy length scale
- $U_{ heta}$  eddy peak velocity (at  $r pprox 0.48 L_E$ )

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- Barotropic eddy:  $\Phi(z) = 1$
- Baroclinic eddy:  $\Phi(z) = \cos(\pi z/H)$  mode one

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- Initialise with  $(u, v) = (-\Psi_y, \Psi_x)$

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$$\Psi=\psi(r)\Phi(z)=-rac{5^{rac{5}{2}}}{64}U_{ heta}L_{E}\mathrm{sech}^{4}\left(rac{r}{L_{E}}
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- Barotropic eddy:  $\Phi(z) = 1$
- Baroclinic eddy:  $\Phi(z) = \cos(\pi z/H)$  mode one
- Initialise with  $(u, v) = (-\Psi_y, \Psi_x)$
- $\bullet\,$  Use cyclo-geostrophic and hydrostatic balances to find  $\rho'$

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Numerical experiment se	tup				

- We let the eddy adjust for 5 tidal periods,  $0 \le t \le 5T$
- Shaded region is relaxed to no-flow





• Then we force a mode-one internal tide at the west boundary

$$u(x = 0, z, t) = U_t \sin(\omega(t - 5T)) \cos\left(\frac{\pi z}{H}\right) R(t - 5T),$$
  
$$5T \le t \le 30T,$$



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Barotropic eddy cases					

Parameter	Value
Barotropic cases:	
$L \times W \times H$	600 km $ imes$ 800 km $ imes$ 5000 m
$N_x \times N_v \times N_z$	1200  imes 1600  imes 25
$\Delta x \times \Delta y \times \Delta z$	0.5 km $ imes$ 0.5 km $ imes$ 200 m
eddy centre	$(x_c, y_c) = (250, 400) \text{ km}$

$\bigvee U_{\theta}$	30	45	60	75	90
LE	cm/s	cm/s	cm/s	cm/s	cm/s
20 km		Х			
30 km	X	X	Х	X	Х
40 km		X			
50 km		X			

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Baroclinic eddy cases					

Parameter	Value
Baroclinic cases:	
$L\timesW\timesH$	720 km $\times$ 400 km $\times$ 5000 m
$N_x \times N_y \times N_z$	1440 $ imes$ 800 $ imes$ 50
$\Delta x \times \Delta y \times \Delta z$	0.5 km $ imes$ 0.5 km $ imes$ 100 m
eddy centre	$(x_c, y_c) = (250, 200) \text{ km}$

	$\bigcup_{\theta}$	30	45	60
LE		cm/s	cm/s	$\rm cm/s$
15	km	Х		
20	km	Х	Х	
25	km	Х	Х	Х
30	km	Х	Х	Х
35	km	Х	Х	Х
40	km	Х	Х	Х
45	km	Х	Х	Х
50	km	Х	Х	Х
55	km	Х	Х	Х

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Normal modes					

• Constant N yields vertical mode solutions following cosine/sine

$$\{\vec{u}_h, p'\} = \{\vec{u}_{h_0}, p'_0\}(x, y, t) + \sum_{n=1}^{\infty} \{\vec{u}_{h_n}, p'_n\}(x, y, t) \cos(m_n z), \\ \{w, \rho'\} = \sum_{n=1}^{\infty} \{w_n, \rho'_n\}(x, y, t) \sin(m_n z),$$

where  $m_n = \frac{n\pi}{H}$ .

• We compute the coefficients from the flow fields by

$$\{\vec{u}_{h_0}, p'_0\} = \frac{1}{H} \int_{-H}^0 \{\vec{u}_h, p'\} \, \mathrm{d}z,$$
  
$$\{\vec{u}_{h_n}, p'_n\} = \frac{2}{H} \int_{-H}^0 \{\vec{u}_h, p'\} \cos(m_n z) \, \mathrm{d}z,$$
  
$$\{w_n, \rho'_n\} = \frac{2}{H} \int_{-H}^0 \{w, \rho'\} \sin(m_n z) \, \mathrm{d}z.$$





- Top: low latitude PSI
- Bottom: mid latitude no PSI



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Baroclinic eddy					

• Density perturbation at modes 2 and 3

• Low f, 
$$L_E = 35$$
 km,  $U_{\theta} = 45$  cm/s,  $t = 16T$ 


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Total pseudo-energy bud	get				

• Review of the total pseudoenergy budget derivation

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Total pseudo-energy bud	get				

- Review of the total pseudoenergy budget derivation
- Start with the hydrostatic Boussinesq equations

$$\begin{aligned} \frac{\partial \vec{u}_h}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \vec{u}_h + f \times \vec{u}_h &= \frac{-1}{\rho_0} \vec{\nabla}_h \rho', \\ \epsilon_{nh} \left( \frac{\partial w}{\partial t} + (\vec{u} \cdot \vec{\nabla}) w \right) &= -\frac{1}{\rho_0} \frac{\partial \rho'}{\partial z} - \frac{g \rho'}{\rho_0}, \\ \frac{\partial \rho'}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \rho' &= \frac{\rho_0 N_0^2}{g} w, \end{aligned}$$

where  $p = \overline{p}(z) + p'$  and  $\rho = \rho_0 + \overline{\rho_1}(z) + \rho'$ .

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Total pseudo-energy bud	get				

- Review of the total pseudoenergy budget derivation
- Start with the hydrostatic Boussinesq equations

$$\begin{split} \frac{\partial \vec{u}_h}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \vec{u}_h + f \times \vec{u}_h &= \frac{-1}{\rho_0} \vec{\nabla}_h p', \\ \epsilon_{nh} \left( \frac{\partial w}{\partial t} + (\vec{u} \cdot \vec{\nabla}) w \right) &= -\frac{1}{\rho_0} \frac{\partial p'}{\partial z} - \frac{g \rho'}{\rho_0}, \\ \frac{\partial \rho'}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \rho' &= \frac{\rho_0 N_0^2}{g} w, \end{split}$$

where  $p = \overline{p}(z) + p'$  and  $\rho = \rho_0 + \overline{\rho_1}(z) + \rho'$ .

• Hydrostatic approximation sets  $\epsilon_{nh} = 0$ 

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Total pseudo-energy bud	get				

## • Dot product between $ho_0 ec{u}$ and the momentum equations

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Total pseudo-energy bud	get				

- Dot product between  $ho_0 \vec{u}$  and the momentum equations
- Multiply density equation by  $\frac{g^2 \rho'}{\rho_0 N_0^2}$

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Total pseudo-energy budget						

- $\bullet\,$  Dot product between  $\rho_0 \vec{u}$  and the momentum equations
- Multiply density equation by  $\frac{g^2 \rho'}{\rho_0 N_0^2}$
- Add the results, integrate over a volume, use some algebra, we get

$$\frac{\mathrm{d}}{\mathrm{d}t}P + W + K_f + A_f = 0$$

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Total pseudo-energy bud	get				

$$\frac{\mathrm{d}}{\mathrm{d}t}P+W+K_f+A_f=0,$$

where

$$\begin{split} P &= \iiint_V \rho_0 \frac{1}{2} (u^2 + v^2) + \frac{g^2 \rho'^2}{2N^2 \rho_0} \, \mathrm{d}V \text{ (total pseudo-energy),} \\ W &= \iint_{\delta V} \rho' \vec{u} \cdot \hat{n} \, \mathrm{d}S \text{ (linear energy flux),} \\ K_f &= \iint_{\delta V} \frac{\rho_0}{2} \vec{u} \cdot \hat{n} (u^2 + v^2) \, \mathrm{d}S \text{ (nonlinear flux of kinetic energy),} \\ A_f &= \frac{g^2}{2\rho_0 N^2} \iint_{\delta V} \rho'^2 \vec{u} \cdot \hat{n} \, \mathrm{d}S \end{split}$$

(nonlinear flux of available potential energy).

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Projection of governing	equations				

• We wish to have an energy budget for each vertical mode

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Projection of governing e	equations				

- We wish to have an energy budget for each vertical mode
- Recall the cosine and sine series:

$$\{\vec{u}_h, p'\} = \{\vec{u}_{h_0}, p'_0\}(x, y, t) + \sum_{n=1}^{\infty} \{\vec{u}_{h_n}, p'_n\}(x, y, t) \cos(m_n z),$$

$$\{w, \rho'\} = \sum_{n=1}^{\infty} \{w_n, \rho'_n\}(x, y, t)\sin(m_n z),$$

where  $m_n = \frac{n\pi}{H}$ .

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• These series are substituted into the horizontal momentum and density equations

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- Recall the cosine and sine series:

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$$\{w, \rho'\} = \sum_{n=1}^{\infty} \{w_n, \rho'_n\}(x, y, t)\sin(m_n z),$$

where  $m_n = \frac{n\pi}{H}$ .

- These series are substituted into the horizontal momentum and density equations
- Then we collect terms at each vertical mode

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Projection of governing	equations				

• The linear terms are straightforward,

$$\begin{split} \frac{\partial \vec{u}_h}{\partial t} &= \frac{\partial \vec{u}_{h_0}}{\partial t} + \sum_{n=1}^{\infty} \frac{\partial \vec{u}_{h_n}}{\partial t} \cos(m_n z), \\ \vec{f} \times \vec{u}_h &= \vec{f} \times \vec{u}_{h_0} + \sum_{n=1}^{\infty} \vec{f} \times \vec{u}_{h_n} \cos(m_n z), \\ \frac{-1}{\rho_0} \nabla_h p' &= \frac{-1}{\rho_0} \nabla_h p'_0 + \frac{-1}{\rho_0} \sum_{n=1}^{\infty} \nabla_h p'_n \cos(m_n z) \end{split}$$

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• The linear terms are straightforward,

$$egin{aligned} rac{\partialec{u}_h}{\partial t} &= rac{\partialec{u}_{h_0}}{\partial t} + \sum_{n=1}^\infty rac{\partialec{u}_{h_n}}{\partial t}\cos(m_n z), \ ec{f} imes ec{u}_h &= ec{f} imes ec{u}_{h_0} + \sum_{n=1}^\infty ec{f} imes ec{u}_{h_n}\cos(m_n z), \ rac{-1}{
ho_0} 
abla_h p' &= rac{-1}{
ho_0} 
abla_h p'_0 + rac{-1}{
ho_0} \sum_{n=1}^\infty 
abla_h p'_n \cos(m_n z). \end{aligned}$$

• The nonlinear terms require a bit of work

$$(\vec{u}\cdot\vec{\nabla})\vec{u}_h=\vec{N}^u=\vec{N}_0^u+\sum_{n=1}^\infty\vec{N}_n^u\cos(m_nz),$$

• Copious use of trig substitution yields

$$\begin{split} \vec{N}_{0}^{u} &= (\vec{u}_{h_{0}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{0}} + \frac{1}{2}\sum_{i=1}^{\infty} (\vec{u}_{h_{i}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{i}} - \frac{1}{2}\sum_{i=1}^{\infty} w_{i}\vec{u}_{h_{i}}m_{i}, \\ \vec{N}_{1}^{u} &= \left[ \left( (\vec{u}_{h_{0}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{1}} + (\vec{u}_{h_{1}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{0}} \right) + \frac{1}{2}\sum_{i=1}^{\infty} \left( (\vec{u}_{h_{i}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{i+1}} + (\vec{u}_{h_{i+1}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{i}} \right) \right] \\ &- \frac{1}{2} \left[ \sum_{i=1}^{\infty} w_{i}\vec{u}_{h_{i+1}}m_{i+1} + w_{i+1}\vec{u}_{h_{i}}m_{i} \right], \\ \vec{N}_{2}^{u} &= \left[ \left( (\vec{u}_{h_{0}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{2}} + (\vec{u}_{h_{2}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{0}} \right) + \frac{1}{2} (\vec{u}_{h_{1}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{1}} \\ &+ \frac{1}{2}\sum_{i=1}^{\infty} \left( (\vec{u}_{h_{i}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{i+2}} + (\vec{u}_{h_{i+2}} \cdot \vec{\nabla}_{h})\vec{u}_{h_{i}} \right) \right] \\ &+ \frac{1}{2} \left[ w_{1}\vec{u}_{h_{1}}m_{1} - \sum_{i=1}^{\infty} (w_{i}\vec{u}_{h_{i+2}}m_{i+2} + w_{i+2}\vec{u}_{h_{i}}m_{i}) \right] \\ \vec{v}^{i} u \end{split}$$

 $\hat{N}_3^u = \dots$ 

Finally, the projected horizontal momentum equation is written as as sum over modes

$$\vec{M}_0 + \sum_{n=1}^{\infty} \vec{M}_n \cos(m_n z) = 0,$$

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where the coefficients of each mode sum to zero,

$$\vec{M}_0 = \frac{\partial \vec{u}_{h_0}}{\partial t} + N_0^u + \vec{f} \times \vec{u}_{h_0} + \frac{1}{\rho_0} \vec{\nabla}_h p_0' = 0,$$
  
$$\vec{M}_n = \frac{\partial \vec{u}_{h_n}}{\partial t} + N_n^u + \vec{f} \times \vec{u}_{h_n} + \frac{1}{\rho_0} \vec{\nabla}_h p_n' = 0, \qquad n = 1, 2, 3, \dots$$

Finally, the projected horizontal momentum equation is written as as sum over modes

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where the coefficients of each mode sum to zero,

$$\begin{split} \vec{M}_0 &= \frac{\partial \vec{u}_{h_0}}{\partial t} + N_0^u + \vec{f} \times \vec{u}_{h_0} + \frac{1}{\rho_0} \vec{\nabla}_h p_0' = 0, \\ \vec{M}_n &= \frac{\partial \vec{u}_{h_n}}{\partial t} + N_n^u + \vec{f} \times \vec{u}_{h_n} + \frac{1}{\rho_0} \vec{\nabla}_h p_n' = 0, \qquad n = 1, 2, 3, \dots \end{split}$$

A similar procedure is used for the density equation,

$$\sum_{n=1}^{\infty} D_n \sin(m_n z) = 0, \text{ which gives}$$
$$D_n = \frac{\partial \rho'_n}{\partial t} + N_n^{\rho} - \frac{\rho_0 N_0^2}{g} w_n = 0, \qquad n = 1, 2, 3, \dots$$

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Modal budgets					

We take the dot product,

$$(\rho_0 H)\vec{u}_{h_0}\cdot\vec{M}_0=0$$

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Modal budgets					

We take the dot product,

$$(\rho_0 H)\vec{u}_{h_0}\cdot\vec{M}_0=0$$

then integrate over an area, employ some algebra, to get

$$\frac{\mathrm{d}}{\mathrm{d}t}K_0 + W_0 + S_0 = 0,$$

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Modal budgets					

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then integrate over an area, employ some algebra, to get

$$\frac{\mathrm{d}}{\mathrm{d}t}K_0 + W_0 + S_0 = 0,$$

where

$$\begin{split} \mathcal{K}_0 &= \rho_0 \frac{H}{2} \iint_A (u_0^2 + v_0^2) \, \mathrm{d}A \quad \text{ is total barotropic kinetic energy,} \\ \mathcal{W}_0 &= H \oint_{\delta A} (\vec{u}_{h_0} \cdot \hat{n}) p_0' \, \mathrm{d}S \quad \text{ is the linear barotropic energy flux, and} \\ \mathcal{S}_0 &= \rho_0 H \iint_A \vec{u}_{h_0} \cdot \vec{N}_0^u \, \mathrm{d}A \quad \text{ is the nonlinear barotropic energy sink.} \end{split}$$

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Modal budgets					

A similar procedure yields the *n*-th baroclinic mode pseudo-energy budget,

$$rac{\mathrm{d}}{\mathrm{d}t} P_n + W_n + S_n = 0, \quad ext{where}$$

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Modal budgets					

A similar procedure yields the *n*-th baroclinic mode pseudo-energy budget,

$$\frac{\mathrm{d}}{\mathrm{d}t}P_n + W_n + S_n = 0, \quad \text{where}$$

$$P_{n} = \rho_{0} \frac{H}{4} \iint_{A} (u_{n}^{2} + v_{n}^{2}) \, \mathrm{d}A + \frac{Hg^{2}}{4\rho_{0}N_{0}^{2}} \iint_{A} \rho_{n}^{\prime 2} \, \mathrm{d}A$$

is the total pseudo energy at mode-n,

$$W_n = rac{H}{2} \oint\limits_{\delta A} (\vec{u}_{h_n} \cdot \hat{n}) p'_n \,\mathrm{d}S,$$

is the linear baroclinic energy flux at mode-n, and

$$S_n = \frac{\rho_0 H}{2} \iint_A \vec{u}_{h_n} \cdot \vec{N}_n^u \, \mathrm{d}A + \frac{Hg^2}{2\rho_0 N_0^2} \iint_A \rho_n N_n^\rho \, \mathrm{d}A,$$

is the nonlinear sink of pseudo-energy at mode-n.

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Energy budget summary					

## The budgets are

Barotropic kinetic energy:

Baroclinic pseudo-energy:

Total pseudo-energy:

$$\begin{aligned} \frac{\mathrm{d}K_0}{\mathrm{d}t} + W_0 + S_0 &= 0\\ \frac{\mathrm{d}P_n}{\mathrm{d}t} + W_n + S_n &= 0\\ \frac{\mathrm{d}P}{\mathrm{d}t} + W + K_f + A_f &= 0 \end{aligned}$$

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Energy budget summary					

## The budgets are

Barotropic kinetic energy:

Baroclinic pseudo-energy:

$$\frac{\mathrm{d}K_0}{\mathrm{d}t} + W_0 + S_0 = 0$$
$$\frac{\mathrm{d}P_n}{\mathrm{d}t} + W_n + S_n = 0$$

Total pseudo-energy:

$$\frac{\mathrm{d}P}{\mathrm{d}t} + W + K_f + A_f \qquad = 0$$

which, as you might expect, sum via

$$\frac{\mathrm{d}}{\mathrm{d}t}K_{0} + \sum_{n=1}^{\infty} \frac{\mathrm{d}}{\mathrm{d}t}P_{n} = \frac{\mathrm{d}}{\mathrm{d}t}P,$$
$$W_{0} + \sum_{n=1}^{\infty} W_{n} = W,$$
$$S_{0} + \sum_{n=1}^{\infty} S_{n} = K_{f} + A_{f}$$

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Energy budget summary					

• The energy budget is computed inside the dashed circle



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Energy budget summary					

• The energy budget is computed inside the dashed circle



Also we have the tidal average operator,

$$ar{X}(t) = rac{1}{T} \int\limits_{t-T}^t X(t) \,\mathrm{d}t, \quad t \geq T,$$

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Focussing and normal mode scattering

Introduction	Methods	Results 1	Energy budgets	Results 2	Summary
No eddy					000000



- Top: low latitude PSI
- Bottom: mid latitude no PSI

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Barotropic eddy					



- Energy flux magnitude
- $|p'_1 \vec{u_1}|$
- $f = 0.5 \times 10^{-4} \text{ s}^{-1}$
- $L_E = 50 \text{ km}$
- $U_{ heta} = 45 \text{ cm/s}.$
- Base flux = 4.78 kW/m.
- Average 15T < t < 16T

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Barotropic eddy					



- Energy flux magnitude
- $|p'_1 \vec{u_1}|$
- $f = 1.0 \times 10^{-4} \text{ s}^{-1}$
- $L_E = 30 \text{ km}$
- $U_{\theta} = 30 \text{ cm/s}.$
- Base flux = 3.68 kW/m.
- Average 16T < t < 17T



• Top:  $U_{\theta} = 45 \text{ cm/s}, L_E = 20, 30, 40, 50 \text{ km}$ 

• Bottom:  $L_E$  = 30 km,  $U_{ heta}$  = 15, 30, 45, 60, 75, 90 cm/s.

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Baroclinic eddy					

- Energy flux normal to 80km radius circle
- $L_E = 35$  km,  $U_{\theta} = 30$ , 45, 60 cm/s

• Average 
$$15T < t < 16T$$



Introduction	Methods	Results 1	Energy budgets	Results 2	Summary	
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Baroclinic eddy induced conversion rates						

• Tidal-averaged terms for low f,  $L_E = 35$  km,  $U_{\theta} = 45$  cm/s







Introduction	Methods	Results 1	Energy budgets	Results 2	Summary
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Baroclinic eddy induced	conversion rates				

$\bigcup_{\theta}$	30	45	60
LE	cm/s	cm/s	cm/s
15 km	Х		
20 km	X	Х	
25 km	X	Х	X
30 km	X	Х	Х
35 km	X	Х	Х
40 km	X	Х	X
45 km	X	Х	X
50 km	X	Х	X
55 km	X	Х	X

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Baroclinic eddy induced conversion rates					



956 1051

60 cm/s
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Baroclinic eddy induced	conversion rates				



200 220

732 805

60 cm/s

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Baroclinic eddy induced	conversion rates				

• Potential weaknesses:

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Baroclinic eddy induced	conversion rates				

- Potential weaknesses:
- The mode-one energy budget includes the eddy and the forced mode-one wave

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Baroclinic eddy induced	conversion rates				

- Potential weaknesses:
- The mode-one energy budget includes the eddy and the forced mode-one wave
- Energy may be lost from the eddy

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Baroclinic eddy induced	conversion rates				

- Potential weaknesses:
- The mode-one energy budget includes the eddy and the forced mode-one wave
- Energy may be lost from the eddy
- However there is no evidence to support this (everything indicates resonance)

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Summary					

Introduction	Methods	Results 1	Energy budgets	Results 2	Summary
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• strongly affect energy flux patterns by creating hot and cold spots of energy flux

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Summary					

- strongly affect energy flux patterns by creating hot and cold spots of energy flux
- use the constructive/destructive interference mechanism, which reduces the coherence of mode-one internal tides

Introduction	Methods	Results 1	Energy budgets	Results 2	Summary
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Summary					

- strongly affect energy flux patterns by creating hot and cold spots of energy flux
- use the constructive/destructive interference mechanism, which reduces the coherence of mode-one internal tides
- are not efficient at scattering energy between internal tide modes

Implications for the background field:

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Summary					

- strongly affect energy flux patterns by creating hot and cold spots of energy flux
- use the constructive/destructive interference mechanism, which reduces the coherence of mode-one internal tides
- are not efficient at scattering energy between internal tide modes

Implications for the background field:

• Stronger energy cascade in hotspots, weaker in cold spots

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Introduction	Methods	Results 1	Energy budgets	Results 2	Summary
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• are efficient at scattering energy to higher internal tide modes

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- are efficient at scattering energy to higher internal tide modes
- use the resonant triad mechanism to scatter energy

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Summary					

- are efficient at scattering energy to higher internal tide modes
- use the resonant triad mechanism to scatter energy
- act as a drag on a mode-one internal tide (analogous to the topographic drag on the barotropic tide)

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Summary					

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Further,

• Low mode internal tides and mesoscale eddies are highly scale-compatible for interaction

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Implications include enhanced localised dissipation:

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Implications include enhanced localised dissipation:

• Energy is shifted from mode-one to mode-two and higher

Introduction	Methods	Results 1	Energy budgets	Results 2	Summary
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Introduction	Methods	Results 1	Energy budgets	Results 2	Summary
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Further,

• Low mode internal tides and mesoscale eddies are highly scale-compatible for interaction

Implications include enhanced localised dissipation:

- Energy is shifted from mode-one to mode-two and higher
- Higher modes propagate slower, subject to more interactions
- Reduces the mode-one energy that reaches a shoreline

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#### Future work

- $\bullet\,$  Extend this work to non-constant N
- Parameterisation?

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Summary					

#### Future work

- Extend this work to non-constant N
- Parameterisation?

# Related questions

 Can mode-two internal tides be observed emanating from an eddy? (satellite measurements, moorings, etc)

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